

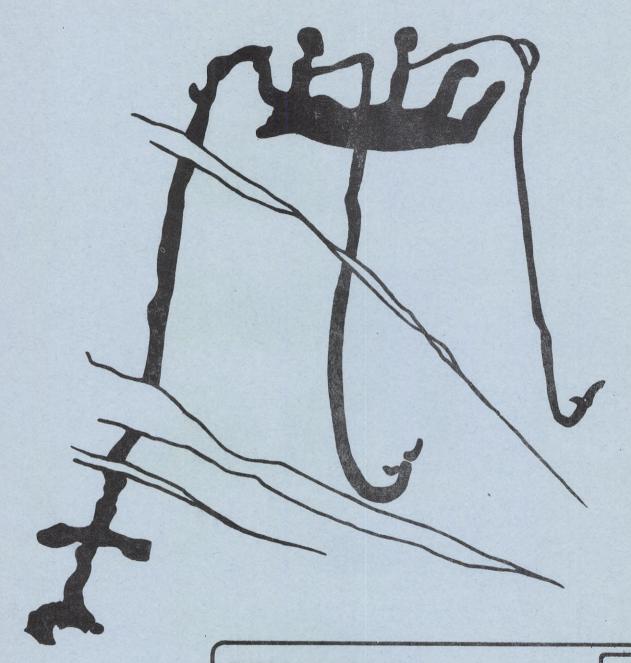
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Odsmål. Kville sn, Bohuslän

Hällristning Fiskare från bronsåldern Rock carving Bronze age fishermen



### MEDDELANDE från HAVSFISKELABORATORIET • LYSEKIL

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Hydrografiska Avdelningen, Göteborg

First Results of a New Numerical Model
for Baltic Water Levels.

by Artur Svansson

November 1970

### First Results of a New Numerical Model for Baltic Water Levels.

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#### 1. Introduction.

Many years ago the author started work on water level problems (Svansson 1959). The Skagerrak, the Kattegatt, the Danish straits and the Baltic were treated as canals. Water levels and water transports were computed by numerical integration, the sectioning being mostly copied from Neumann (1941). Later the method was improved by using e.g. a better sectioning (Svansson 1966) of some parts of the system.

The old numerical system was an explicit one allowing timesteps of approximately 15 minutes. The system presented here is an implicit one aiming at the use of large timesteps, e.g. 24 hours. While it seems possible to get a stable implicit model with the old system of equations, it is not quite clear if the introduction of the new damping term tested here upsets the stability or not. The results presented in this paper, however, do not seem to be influenced by such a possible instability.

#### 2. The system of equations.

$$\frac{\partial \mathcal{U}}{\partial t} = -g A \frac{\partial h}{\partial x} + b T_w - b T_B + \frac{\partial}{\partial x} K \frac{\partial \mathcal{U}}{\partial x}$$

$$\frac{\partial h}{\partial t} = -\frac{1}{b} \frac{\partial \mathcal{U}}{\partial x}$$

$$\frac{\partial h}{\partial t} = -\frac{1}{6} \frac{\partial \mathcal{U}}{\partial x}$$

#### 3. Notations:

= Index of timestep

= Index of sction

U	= Transport of water		$m^3/s$
g	= Acceleration of gravity		m/s <sup>2</sup>
A	= Cross sction area		m <sup>2</sup>
р	= Width of sction		m
h	= Variation of water level		m
q	= Density		t/m <sup>3</sup>
7'	= Turbulent stress component		$t/m$ and $s^2$
7	= <b>7</b> /q		m <sup>2</sup> /s <sup>2</sup>

In this paper the windstress  $\mathcal{L}_{\mathcal{A}} = \mathcal{L}_{\mathcal{A}}$  and the bottom stress  $\mathcal{L}_{\mathcal{A}} = \mathcal{L}_{\mathcal{A}}$ . In all the computations so far, however,  $\mathcal{L}_{\mathcal{A}} = 0$ .

The introduction of the term  $\frac{3}{5\chi} \times \frac{3U}{3\chi}$  is an experiment. As pointed out in Svansson (1968) the tests with a damping term of the type 3U did not fully come up to expectations, nor did the trial with the scheme of Platzman (1963). The K:s used were determined in the following way: The mean salinity from surface to bottom was determined from Granquist (1938) and Anon. (1933) for the period April-October (See Fig. 2). Using the assumption that  $ZS = AK'\frac{3S}{3\chi}$  (Boicourt 1969) is valid (Z = fresh water supply in  $M^3/S$  during the same period of the year taken from Brogmus 1952) the K':s were determined for every section (Fig. 3). They are presented in Table 1. The idea is now to assume that K = KAK', where K is independent of the section but adjustable in order to give the best identity with nature.

4. The Numerical System is presented as an Appendix.

#### 5. Results.

The reason for publishing results already is that one of the first tests is rather interesting. The water levels of Smögen (approximately section 3:2) were introduced as boundary condition  $h_{1/2}$  at the open end of canal 3. No wind was applied; k=0.001 was found to be a good choice. Fig. 4 shows the result of  $h_{\rm G}$  compared with the measured levels at Landsort. The agreement is rather good and could probably be made better by working more carefully:

- 1) Checking the stability. Hints have been given by H. Sundquist (personal communication). The possible instability comes from the open end, section 3:0, but seems to be filtered away in the Danish straits.
- 2) Applying the real boundary condition at section 3:0 and not the levels at Smögen (3:2).
- 3) Studying the new damping term extensively.
- 4) Introducing branching also in the Danish straits as was done in Svansson (1966).
- 5) Applying the actual winds.

#### 6. Discussion.

Fig 5 shows the variations of a) the atmospheric pressure in Stockholm, b) the water level in Smögen c) the water level in Landsort and d) the surface salinity in Kattegatt (approximately section 3:12) during the period concerned. While the level of Smögen approximately follows

the variations in atmospheric pressure the salinity of Kattegatt approximately follows the level of Landsort.

The explanation might be that the large scale variations of the level of the Baltic (Hela 1944 has shown that the levels of Landsort can be used rather well to represent the whole Baltic) are mostly a function of the level at the mouth, but the Kattegatt and the Danish straits filter and damp a large amount of the signal. The variation of the Kattegatt surface salinity which is due to horizontal movements should then probably follow the variations of the Baltic. As Hela (1944) shows transports due to level variations might often amount to 200 000 m<sup>3</sup>/s in the Danish straits and if this goes on for e.g. 10 days it corresponds to a movement of approximately 75 km, if the water moves homogenously, but 150 km if only the 15 m deep surface layer takes part in the transport. Fig. 6 shows that also the surface salinities at the Bornö station (approximately section 3:2) are influenced by the same phenomenon. This relation does not, however, appear that clearly.

Fig. 7 shows the events at a well known occasion, e.g. the large inflow of salt water to the Baltic 1951 (Wyrtki 1954, Fonselius 1962).

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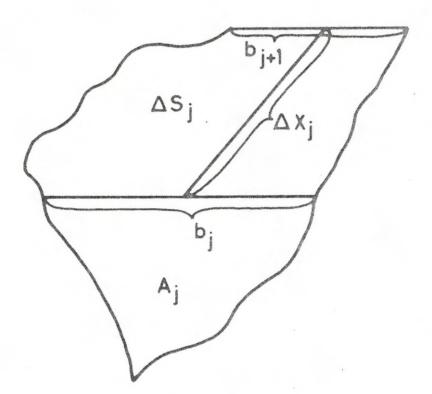
Svansson, A., 1968: Determination of the Wind Stress Coefficient by Water Level Computations II. Medd. fr. Havsfiskelab.,

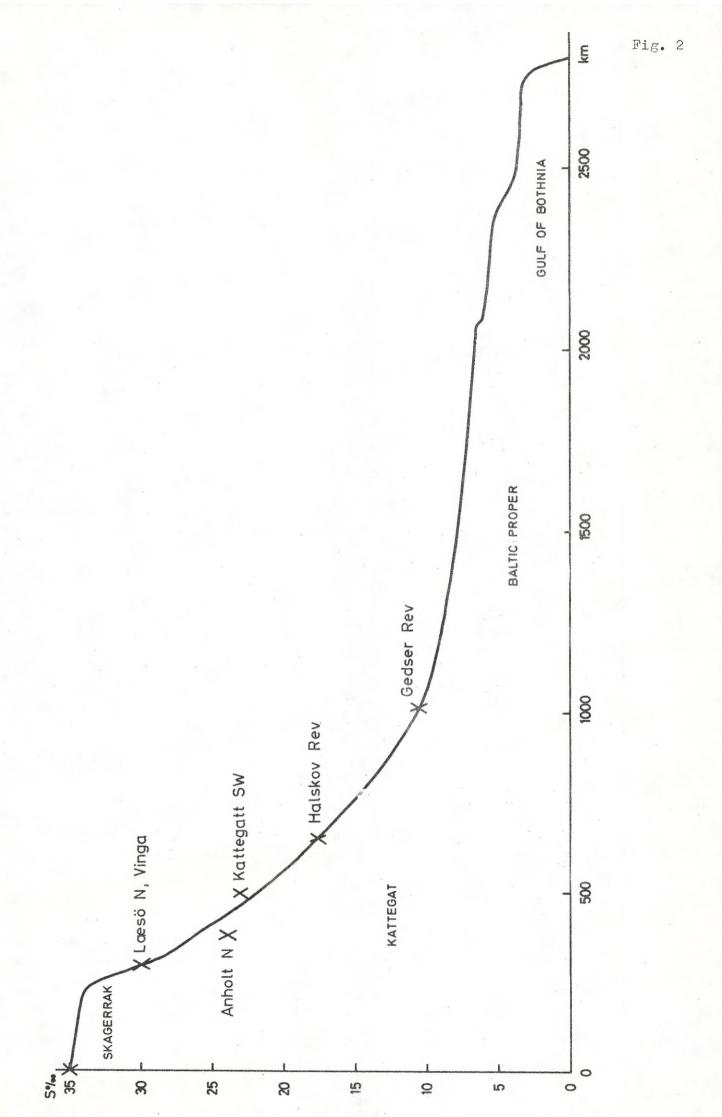
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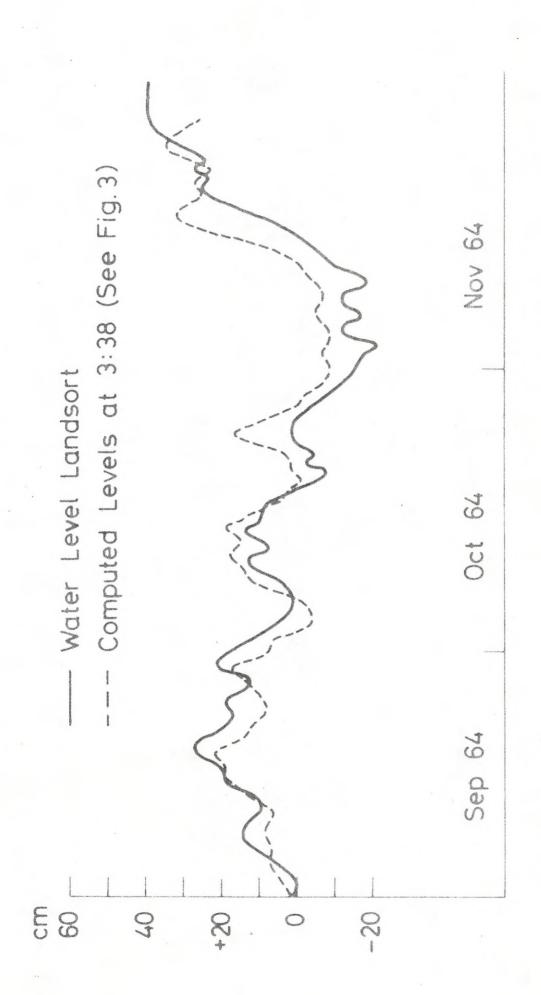
Wyrtki, K., 1954: Der grosse Salzeinbruch in die Ostsee im November und Dezember 1951. Kieler Meeresforsch. X:1, p 19.

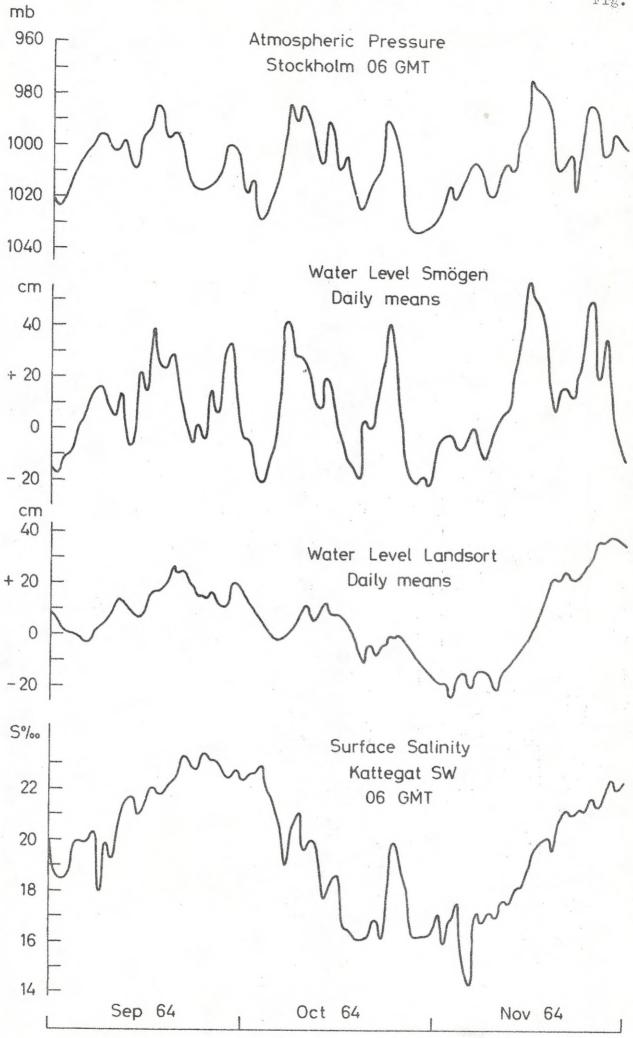
# Table 1. K' in $m^2/s$

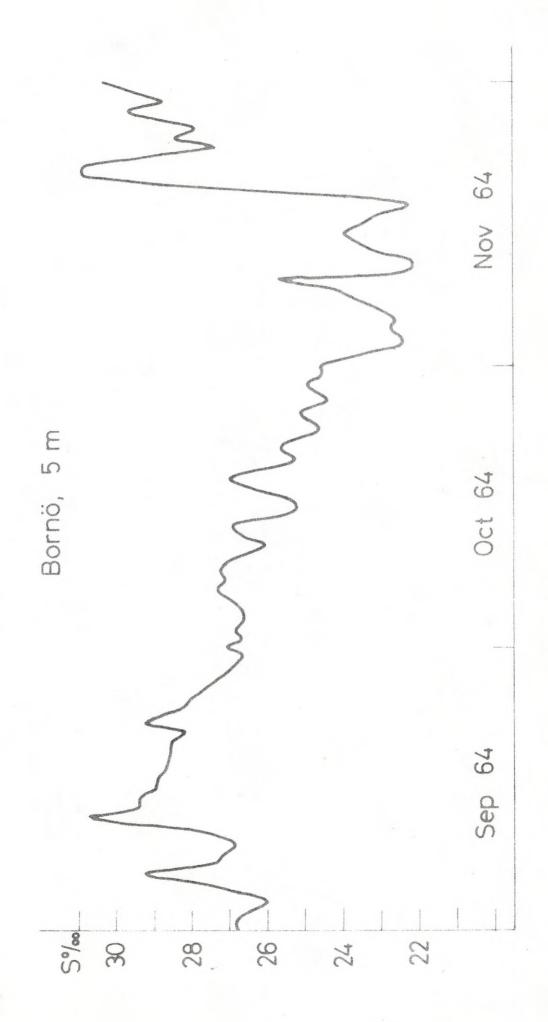
Branch	1	2		3
Section				
0	0	0		4300
1	169	628		4300
2	79	406		2552
3	573	376		3091
4	641	637		4281
5	737	1677		5005
6	2243	1645		5379
7	4600	2280		5485
8	4703			3804
9	2468			4483
10	479			5236
11	211			6749
12	145			9424
13	146			16410
14	227			13880
15	519			10590
16	1545		7.7	34210
17	1704			38395
18	2243			31580
19	746			62230
20	964			51690
21	1000			22180
22				56380
23				12640
24				16420
25				28490
26				37020
27				, 9005
28				12810
29				17720
30				33600
31				22230
32				10305
33				5090
34				4535
35				2120
36				1345
37				1760
38				2000

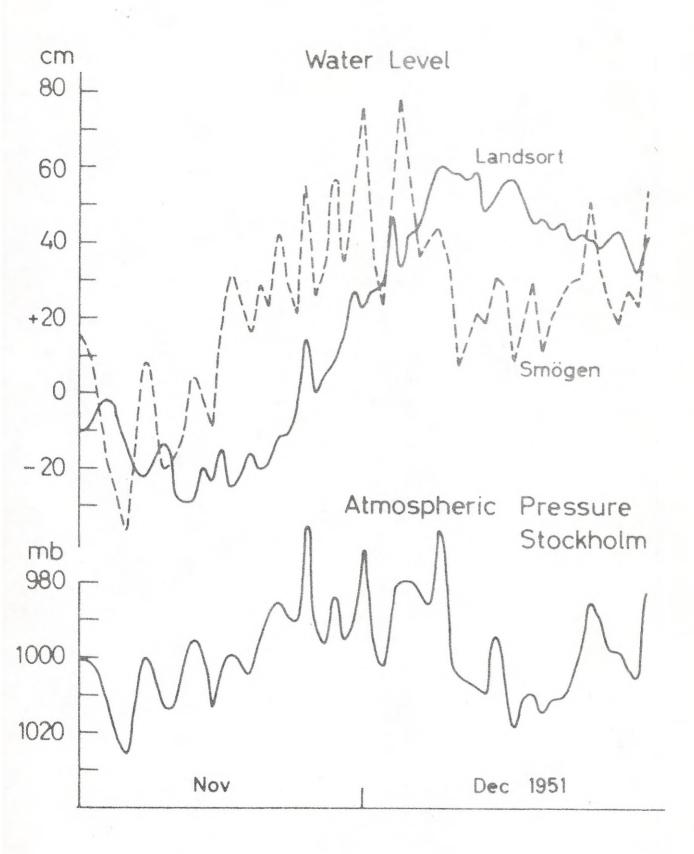












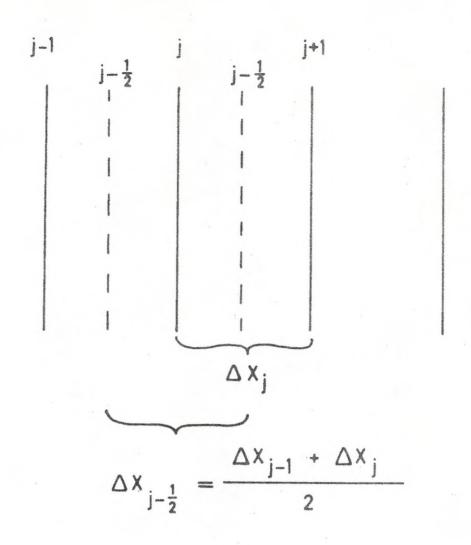
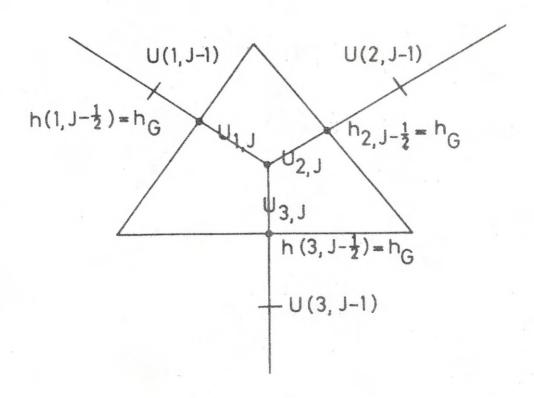


Fig. 8



1,+1 + U" - U" - U"

See Fig. 8

$$U_{i}^{n+1}-U_{i}^{n}=-\frac{gA_{i}}{4k_{i}}\frac{4k_{i}}{(h_{i+\frac{1}{2}}+h_{i+\frac{1}{2}}-h_{i-\frac{1}{2}}-h_{i-\frac{1}{2}})-\beta_{i}\cdot\Delta t}\frac{U_{i}^{n+1}}{2}$$

$$+ \frac{K_{j+\frac{1}{2}} \cdot \Delta t}{2 \Delta K_{j-1} \cdot \Delta K_{j+\frac{1}{2}}} \cdot \frac{\Delta t}{U_{j+\frac{1}{2}} \cdot \Delta t} \cdot \frac{U_n}{U_n} \cdot \frac{K_{j+\frac{1}{2}} \cdot \Delta t}{(2 \Delta K_{j-\frac{1}{2}} \cdot \Delta K_{j-\frac{1}{2}} \cdot \Delta K_{j-\frac{1}{2}} \cdot \Delta K_{j-\frac{1}{2}}) \cdot U_n}{(2 \Delta K_{j-\frac{1}{2}} \cdot \Delta K_{j-\frac{1}{2}} \cdot \Delta K_{j-\frac{1}{2}} \cdot \Delta K_{j-\frac{1}{2}}) \cdot U_n}$$

$$m_{i}h_{i+1}^{i+1} = m_{i}h_{i-1}^{i} - m_{i}f_{i}(u_{i}^{i} - u_{i}^{i}) - m_{i}f_{i}(u_{i}^{i} - u_{i}^{i}) - m_{i}f_{i}(u_{i}^{i} - u_{i}^{i})$$

Bilt With - 2 Li, + r. With - (r. + x.) · W. + x. W. + 

D. = Un (m; t; + r;) - U, (++m; t; +m; t; + 2,4t +5+i)

1 (m; 1; +12) 2m; (h; 4-h; 1) + 6; 4+ 7; 1) + 6; 4+ 7; 1) + 6;

## Richtmyer and Morton (1967):

$$E_{j} = \frac{P_{j}}{Q_{j} - C_{j} E_{j-1}}$$

$$F_{i} = \frac{D_{i}^{n} + P_{i} F_{i-1}}{Q_{i} - C_{i} E_{i-1}}$$

## Branch 1 and 2:

Branch 3: Hat given

$$\frac{U_o^{n+1} + U_o^{n} - U_o^{n-1} - U_o^{n}}{2 b_{j+1} \Delta l_o} = \frac{H_{\underline{t}}^{m} - H_{\underline{t}}^{n}}{\Delta t}$$

$$E_{\circ}=1$$
,  $F_{\circ}$ 

The Branching Point (See Fig. 9
NB. Algol notations):

$$U(L,J-1) = E(L,J-1) * U(L,J) + F(L,J-1)$$
  
 $h_{G}^{**} = h_{G}^{*} - \ell(L,J-1) * (U'(L,J) - U'(L,J-1))$   
 $-\ell(L,J-1) * (U''(L,J) - E(L,J-1) * U'''(L,J)$   
 $-F(L,J-1));$ 

or 
$$h_{G}^{n+1} = h_{G}^{n} - \ell(L,J-1)*(U'(L,J)-U'(L,J-1)-F(L,J-1))$$

$$-U^{n+1}(L,J)*\ell(L,J-1)*(I-E(L,J-1));$$

$$LE(L)$$

### Therefore from the system

$$\begin{cases} h_G^{n+1} = T(L) - U^{n+1}(L,J) * LE(L) & 3ekv:s \\ U^{n+1}(I,J) + U^{n+1}(2,J) + U^{n+1}(3,J) = 0 \end{cases}$$
all  $U^n(I,J)$  and also  $h_G^{n+1}$  can be determined.

Then
$$U_{J-1} = E_{J-1}U_J + F_{J-1} \quad \text{etc backwards.}$$

Finally
$$h_{j+\frac{1}{2}}^{n-1} = h_{j+\frac{1}{2}} - \ell_{j} \left( U_{j+1} - U_{j}^{n} + U_{j+1}^{n-1} - U_{j}^{n-1} \right)$$

